

The Tribological Behaviours of New and Existing Self-lubricating Materials for Space

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(ESTL)

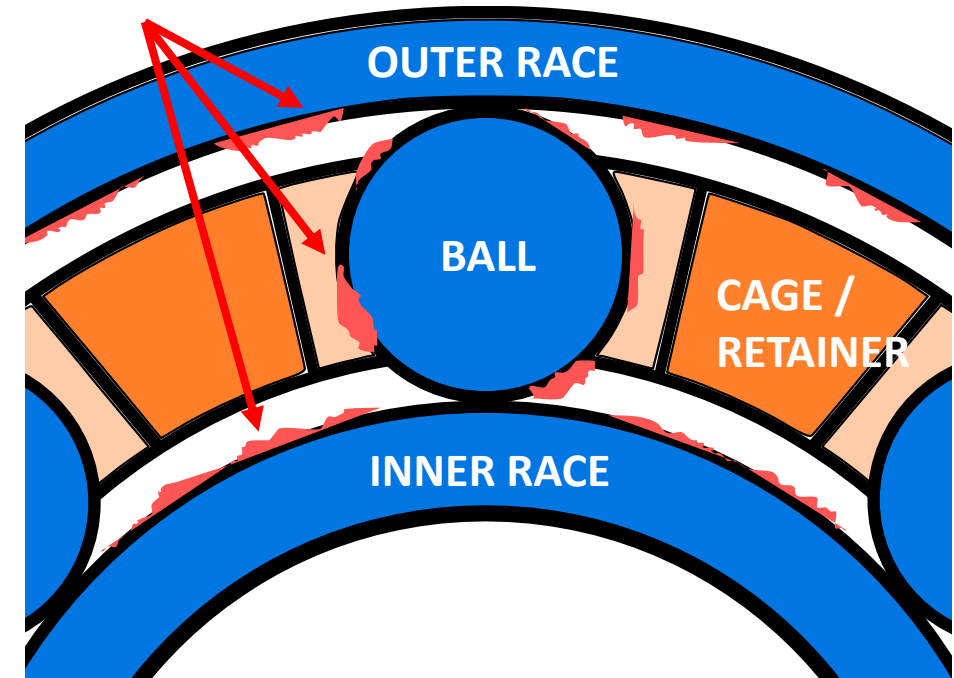
European Space Mechanisms and Tribology
Symposium

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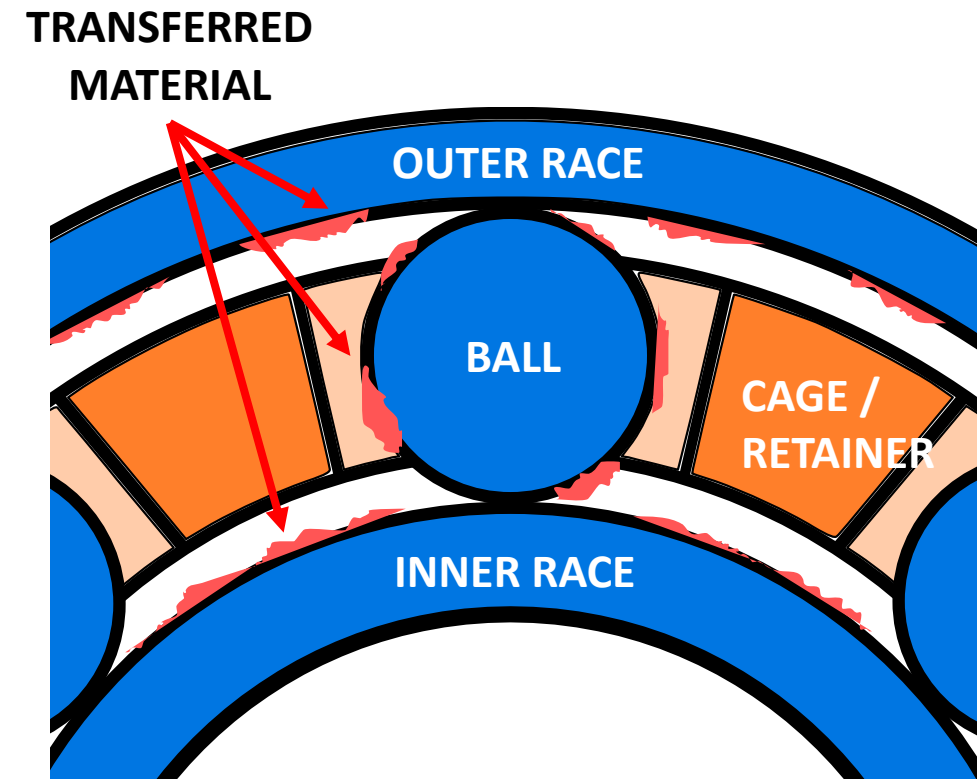
Double Transfer Mechanism

**TRANSFERRED
MATERIAL**



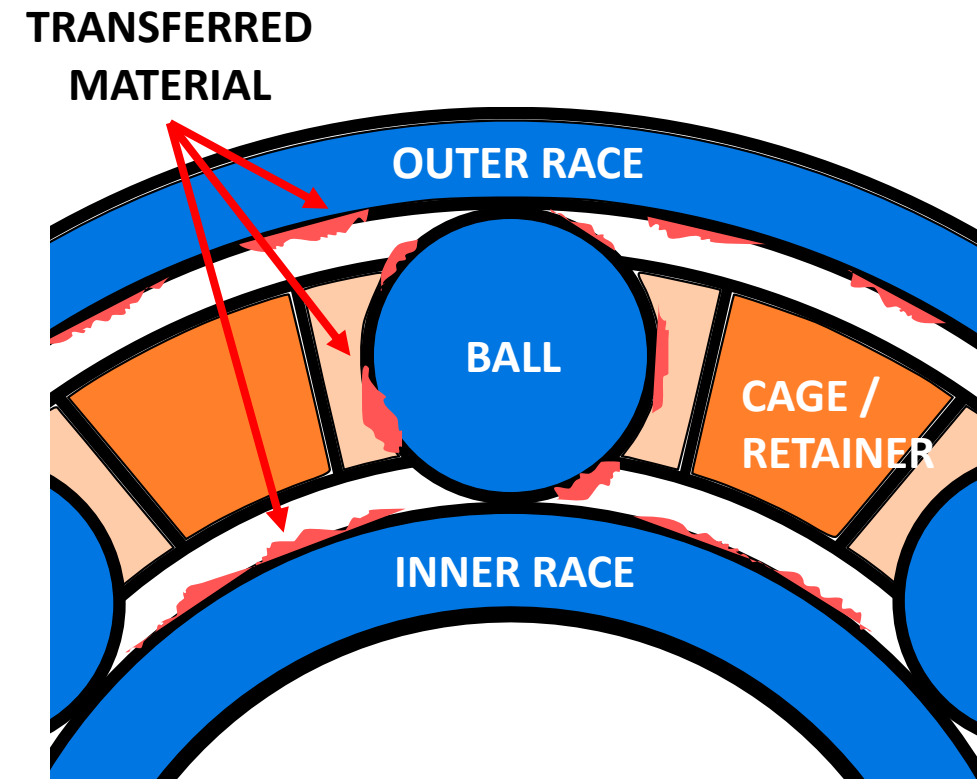
Double Transfer Mechanism

- Bearing parts coated in solid film:
 - MoS₂
 - Lead



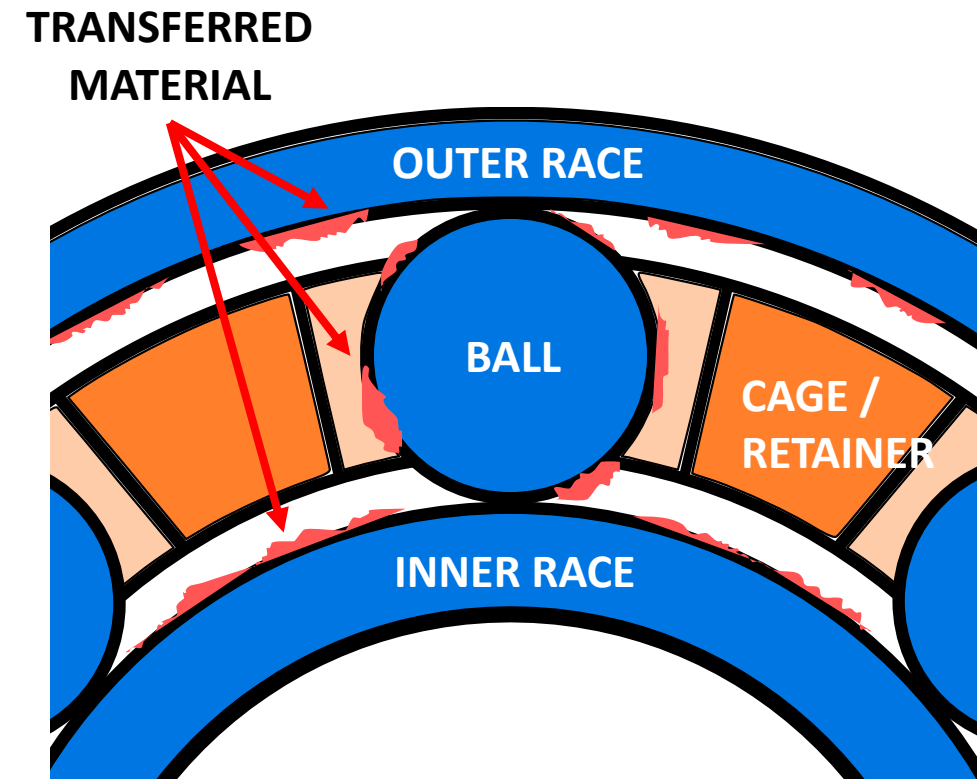
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 - PGM-HT
 - Lead/Bronze



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 - Lead/Bronze
- Cage -> Ball -> Raceway



SLM History

MoS₂
RT/Duroid
5813

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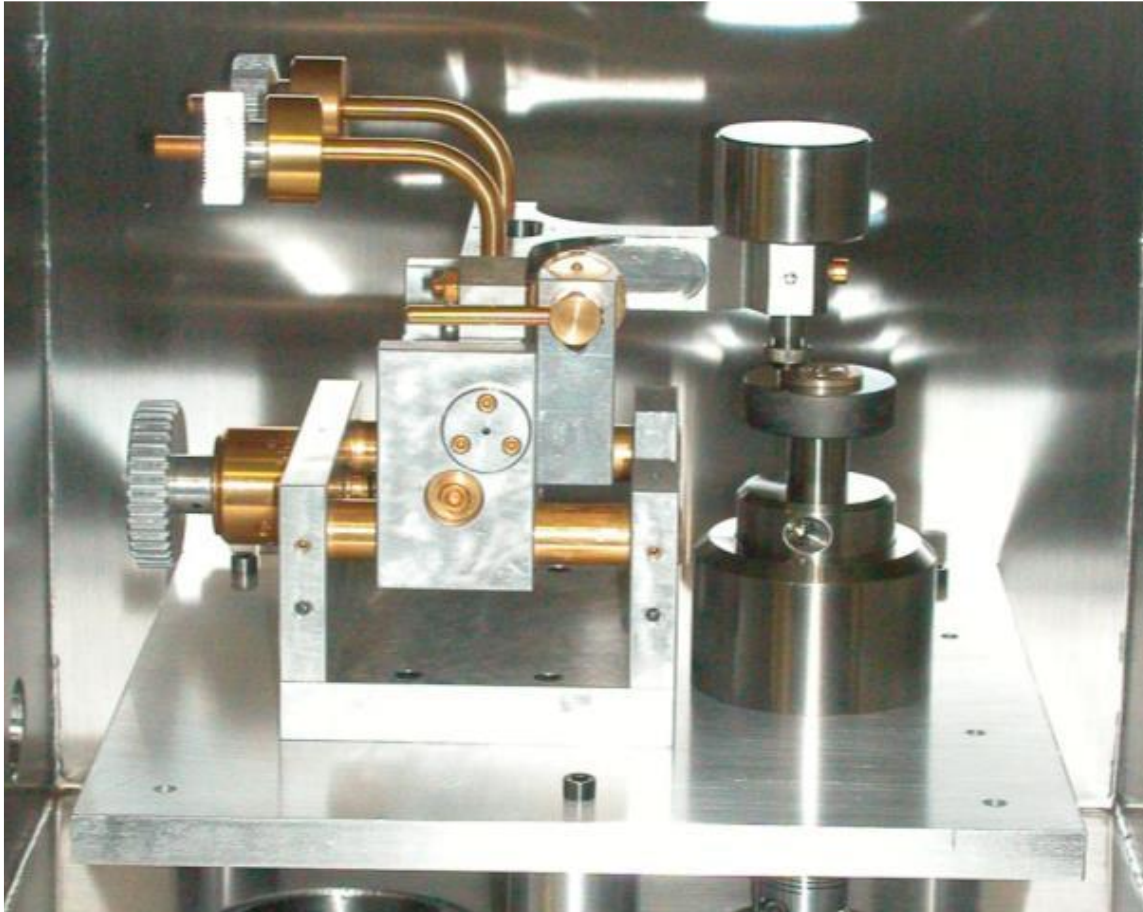
MoS₂
???

SLM History

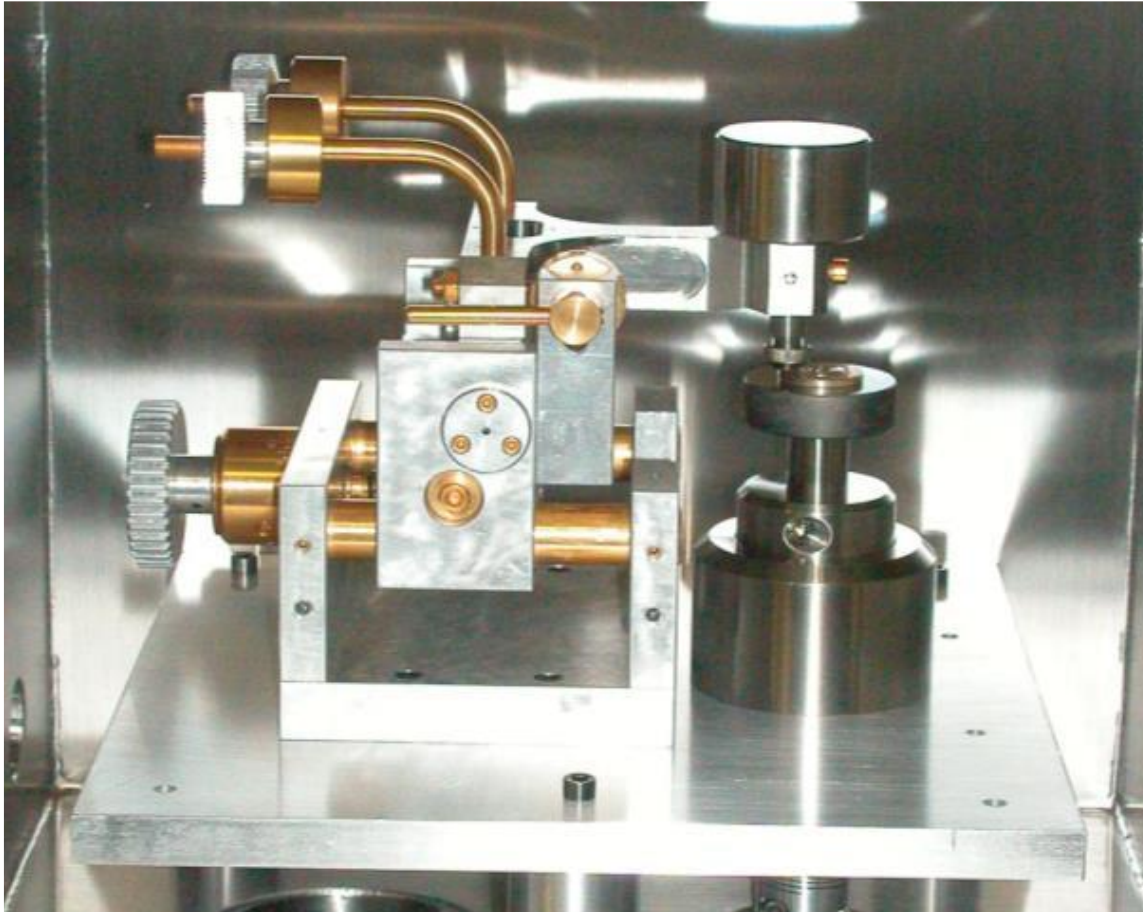


- Similar or better friction performance than PGM-HT
- Resistant to operation in air
- EU sourced

Traditional Methods

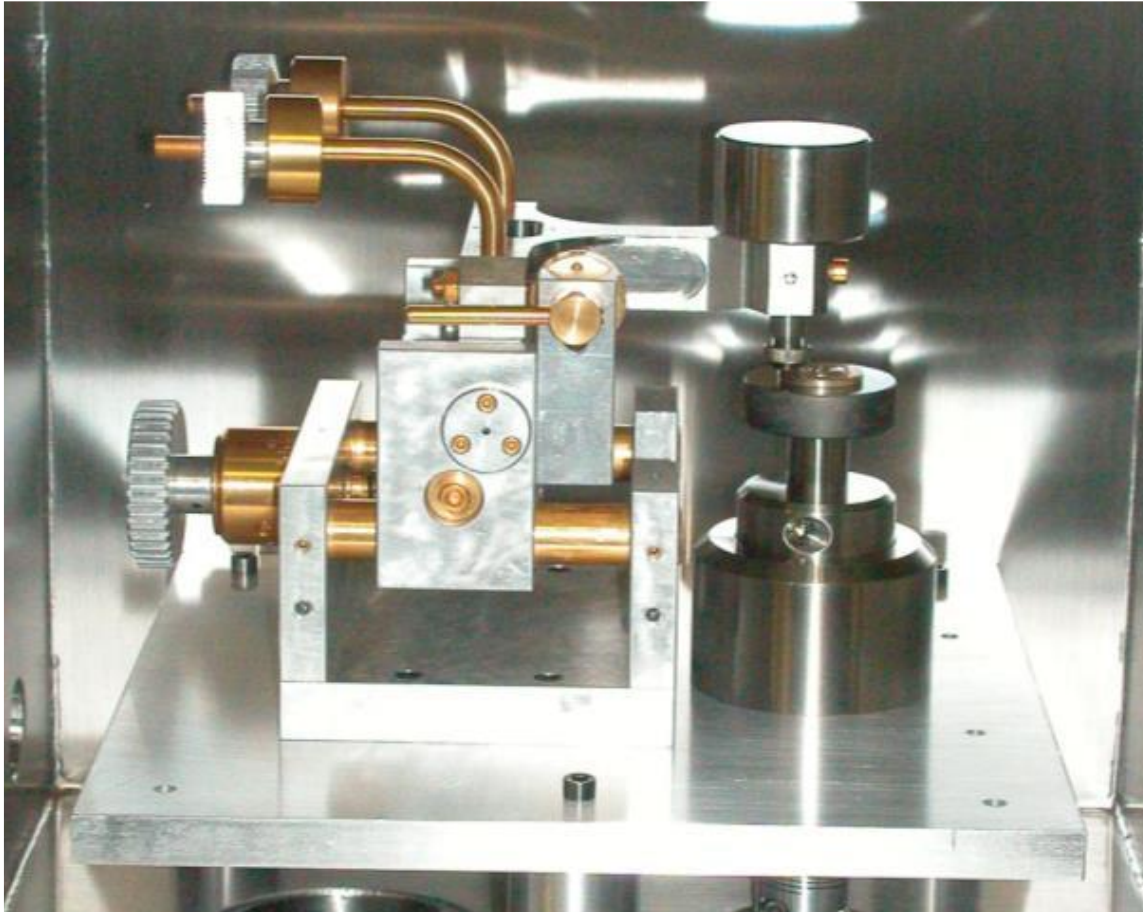


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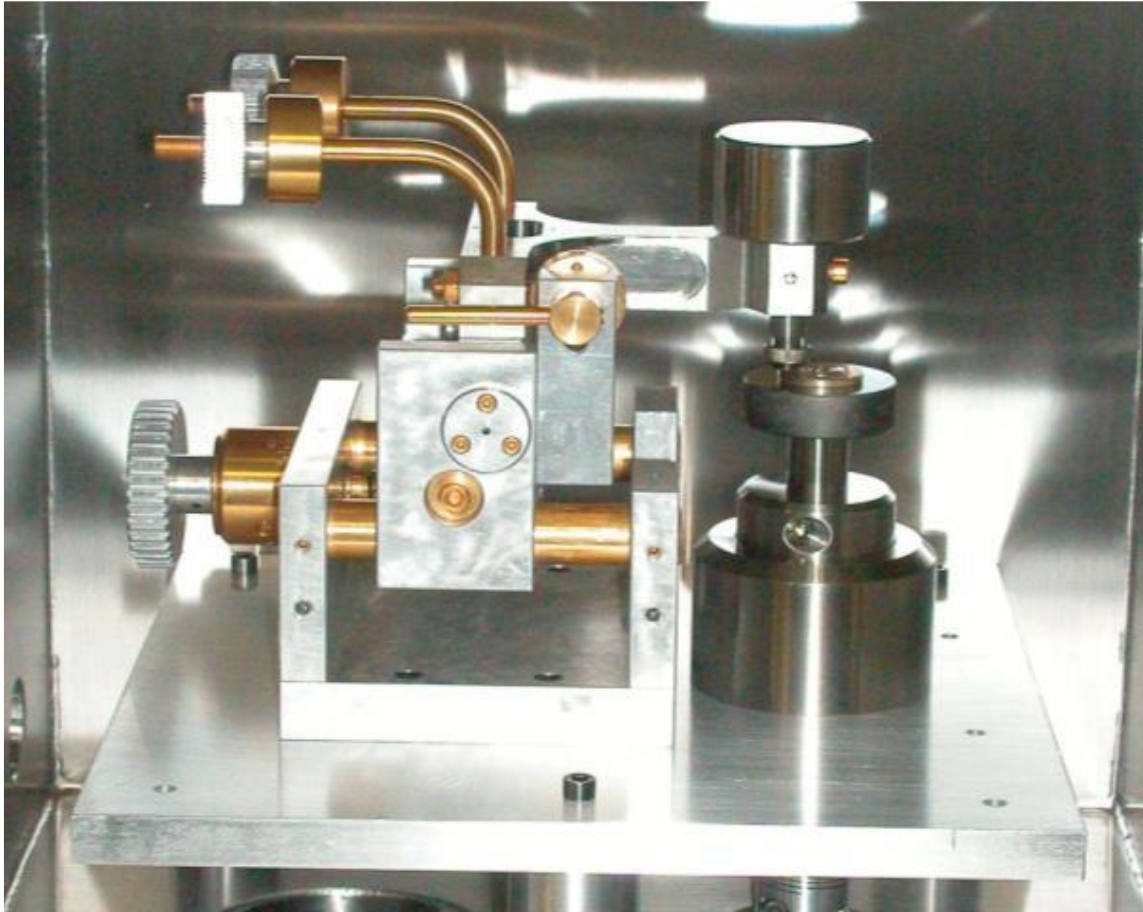
- Pin made of SLM against steel disc

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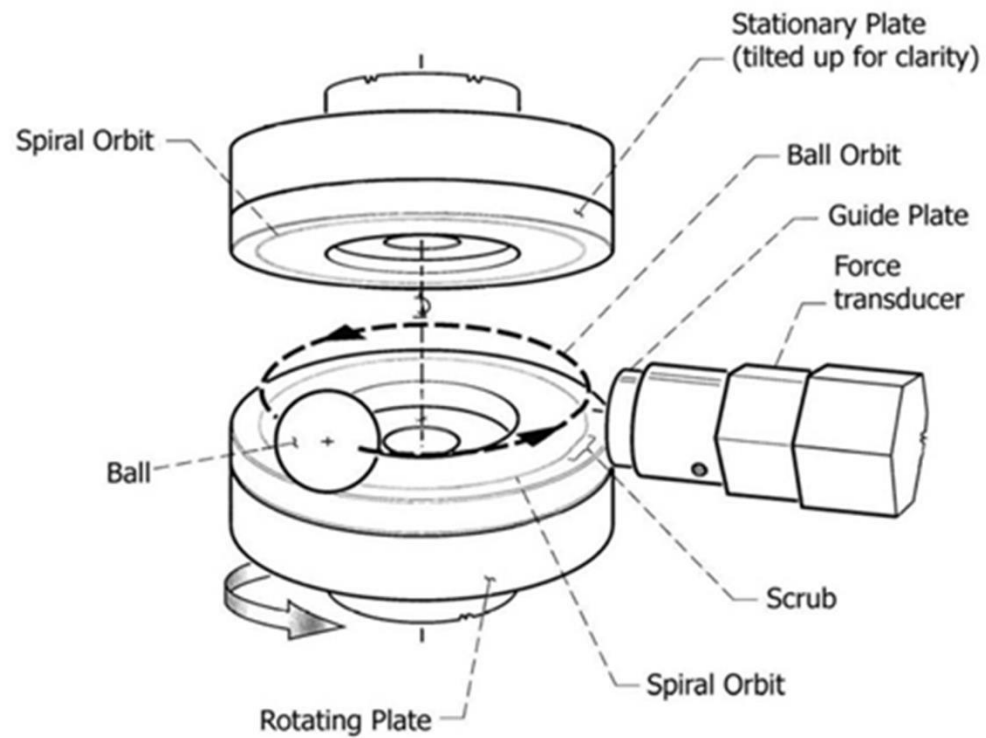
- Pin made of SLM against steel disc
- Easily change:
 - Load
 - Temperature
 - Sliding Speed
 - Environment

Traditional Methods



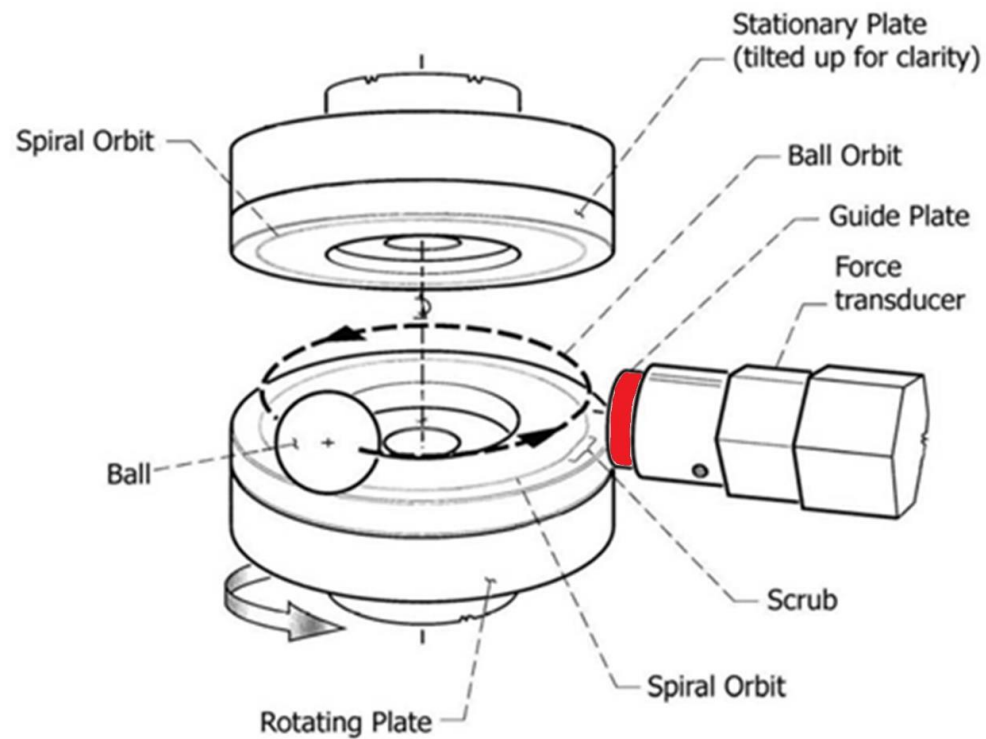
- Pin made of SLM against steel disc
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- Sliding representative of cage/ball contact but not double transfer mechanism

Spiral Orbit Tribometer

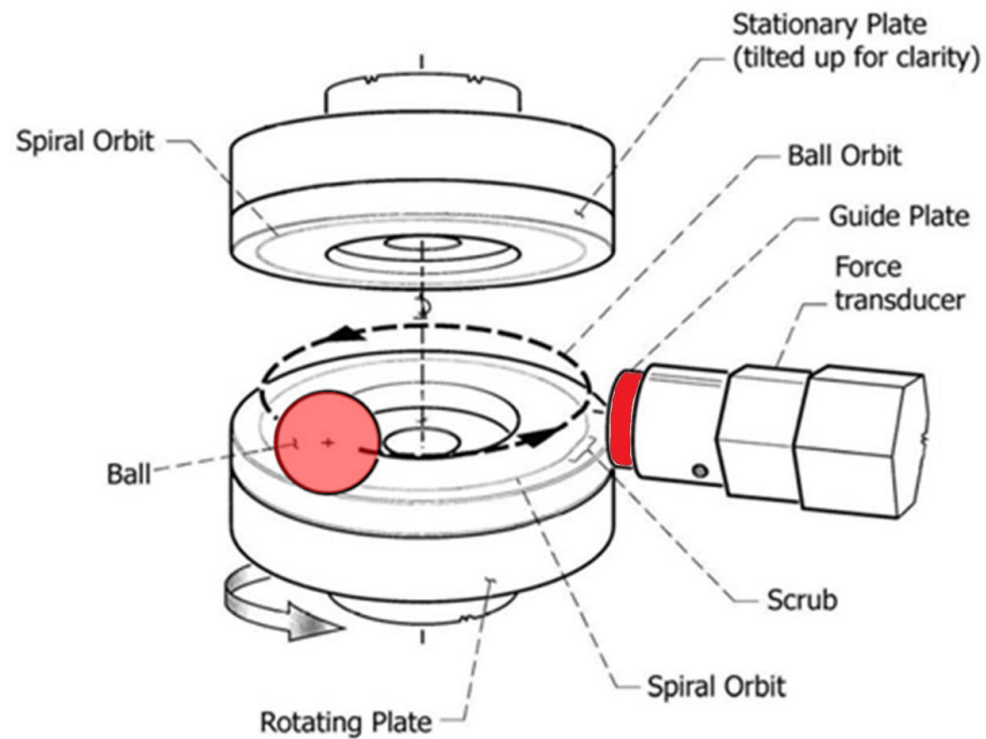


Spiral Orbit Tribometer

- Guide plate manufactured from SLM

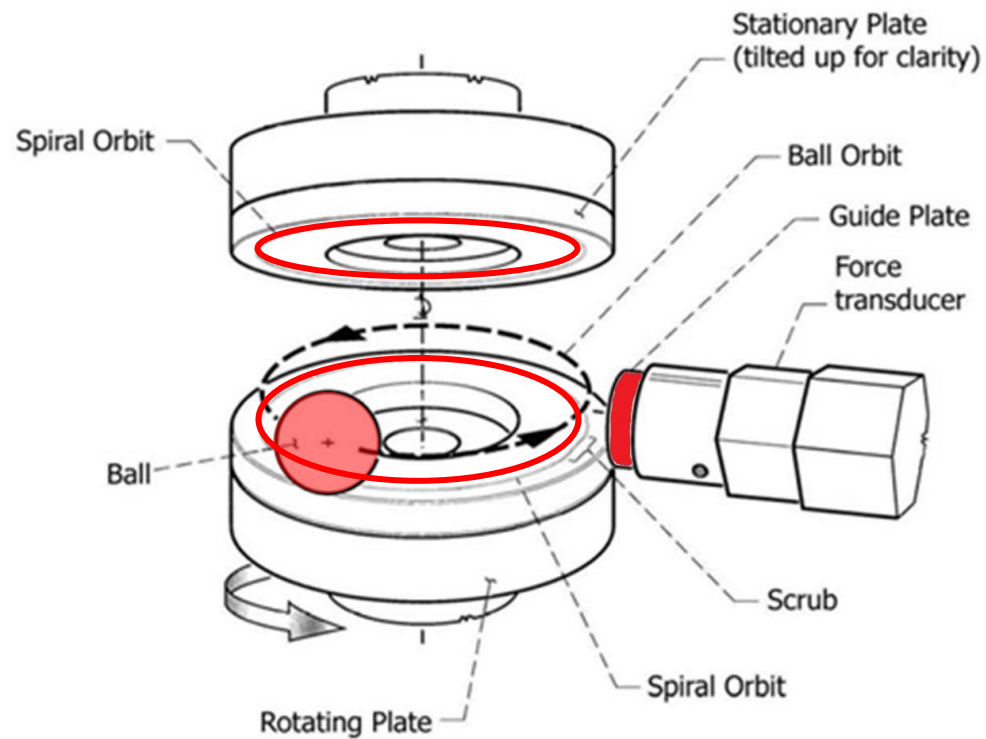


Spiral Orbit Tribometer



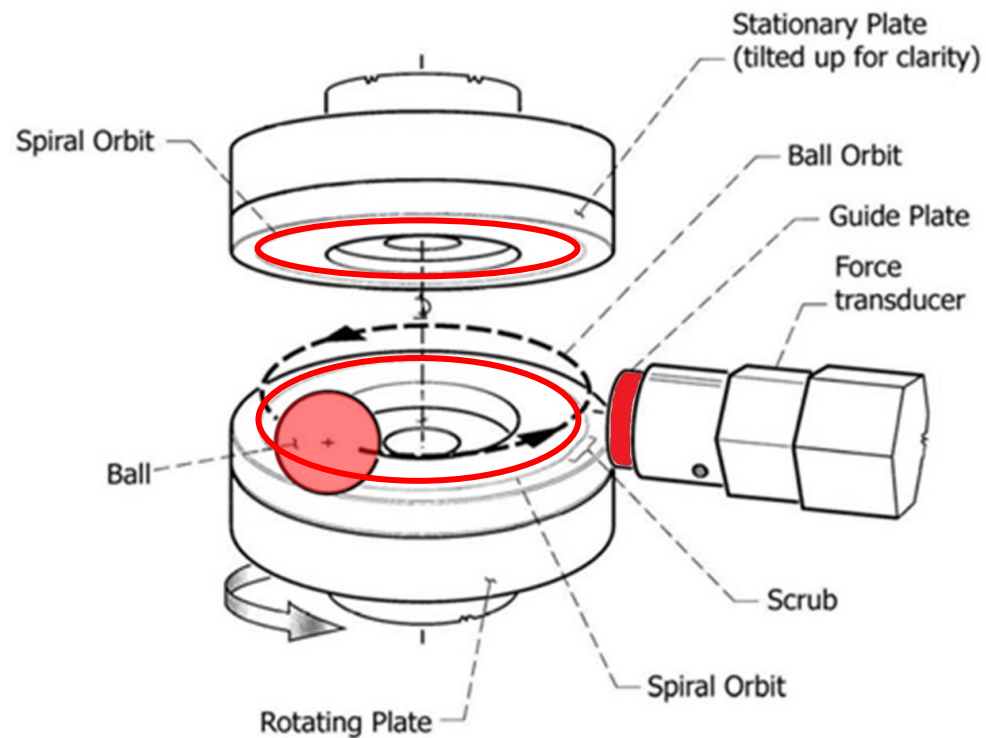
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- Material transfers to ball during collision with guide plate

Spiral Orbit Tribometer



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- Material transfers to plate from ball

Spiral Orbit Tribometer



- Guide plate manufactured from SLM
- Material transfers to ball during collision with guide plate
- Material transfers to plate from ball
- Allows for examination of transfer film formation on plates

SOT Test Results

Material	CoF (Mean)	CoV	Mo Thickness (um)
RT/Duroid 5813	0.270	41.5%	0.362
PGM-HT	0.187	53.6%	0.359
TSE8591	0.211	55.2%	0.353
C79	0.301	26.5%	0.356
Vespel SP3	0.498	26.8%	0.383
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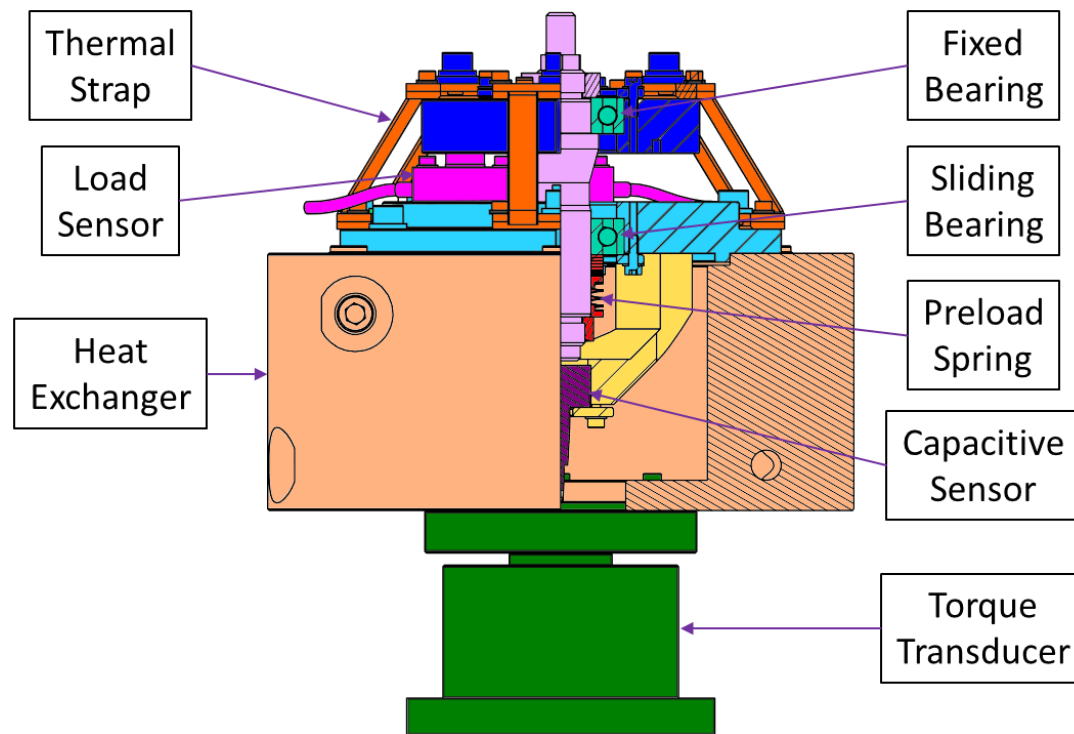
- PGM-HT/TSE8591 have similar friction properties
- Mo XRF measurements indicate stable film formation on balls

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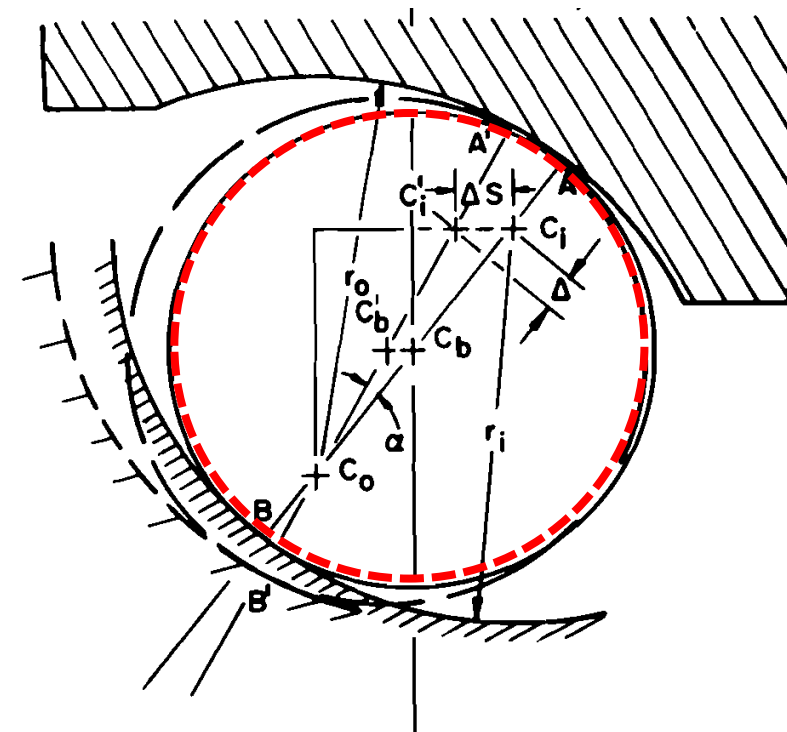
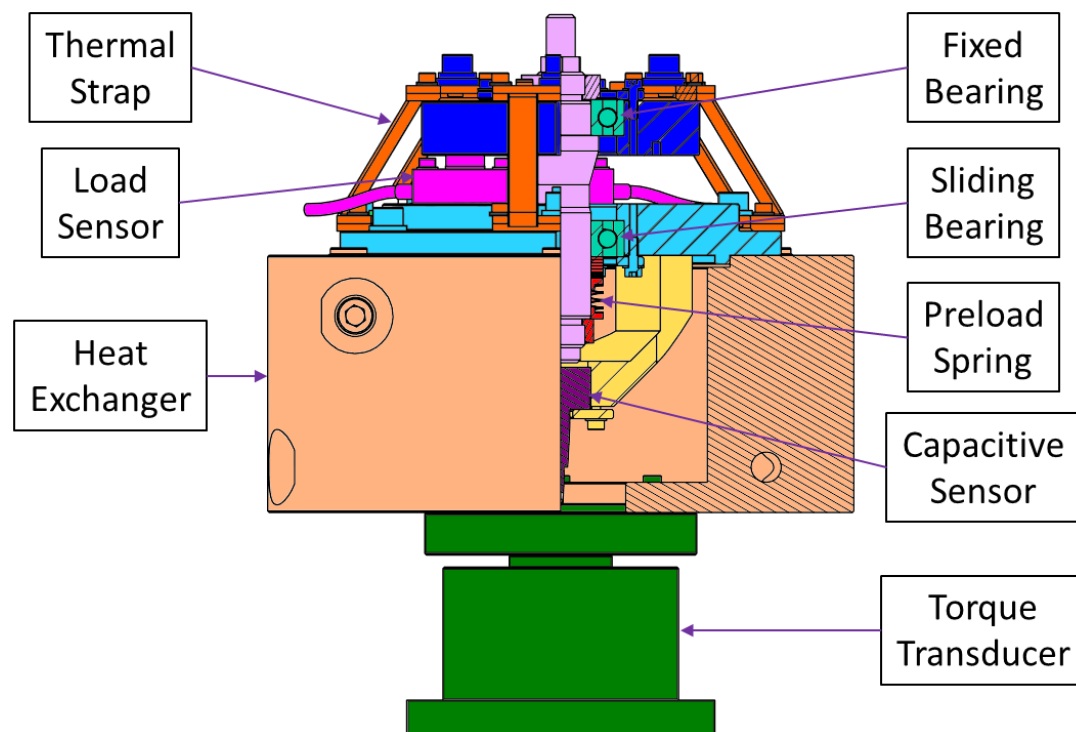
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- PGM-HT/TSE8591 have similar friction properties
- Mo XRF measurements indicate stable film formation on balls
- Post test inspections show PGM-HT film highly variable compared to uniform homogenous films of Duroid/TSE8591

Advanced Bearing Test Rig

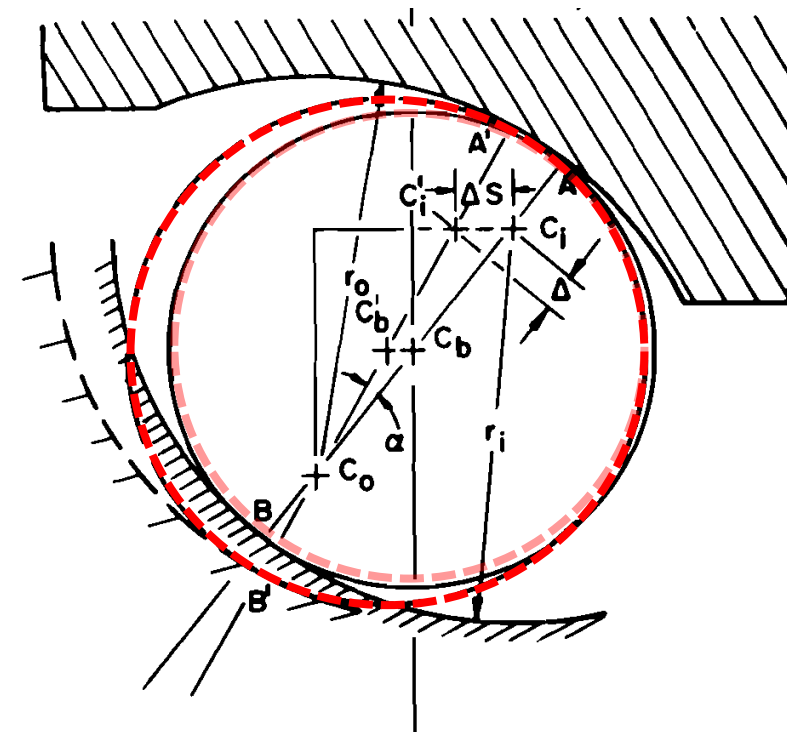
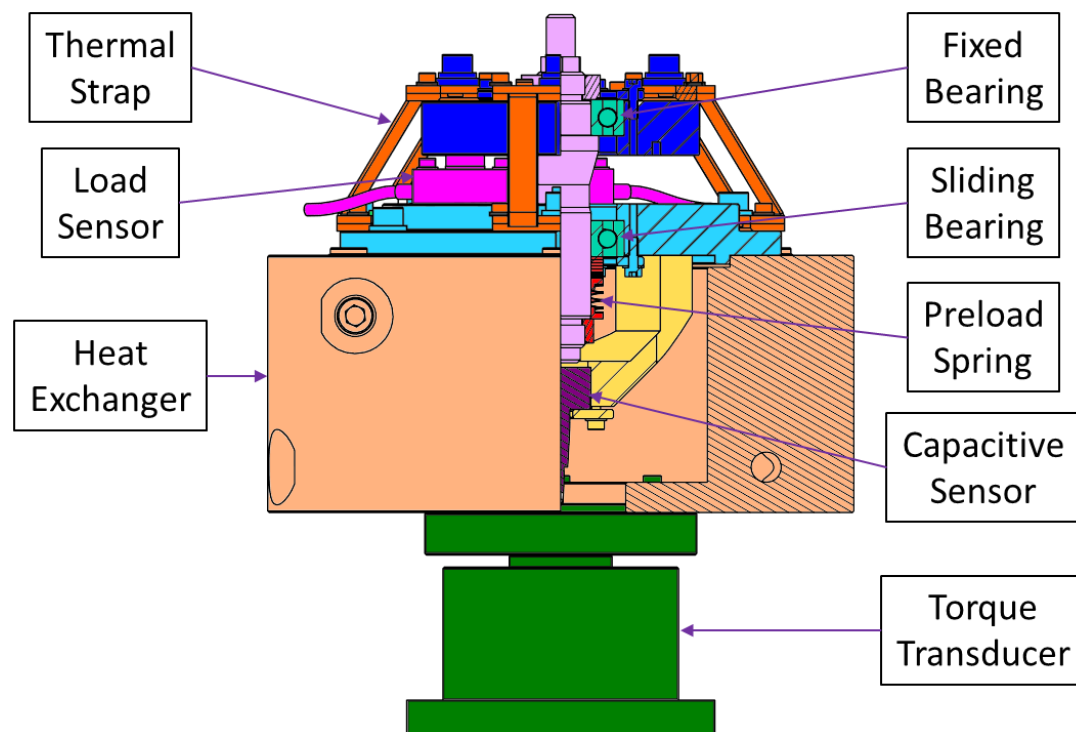


ABTR



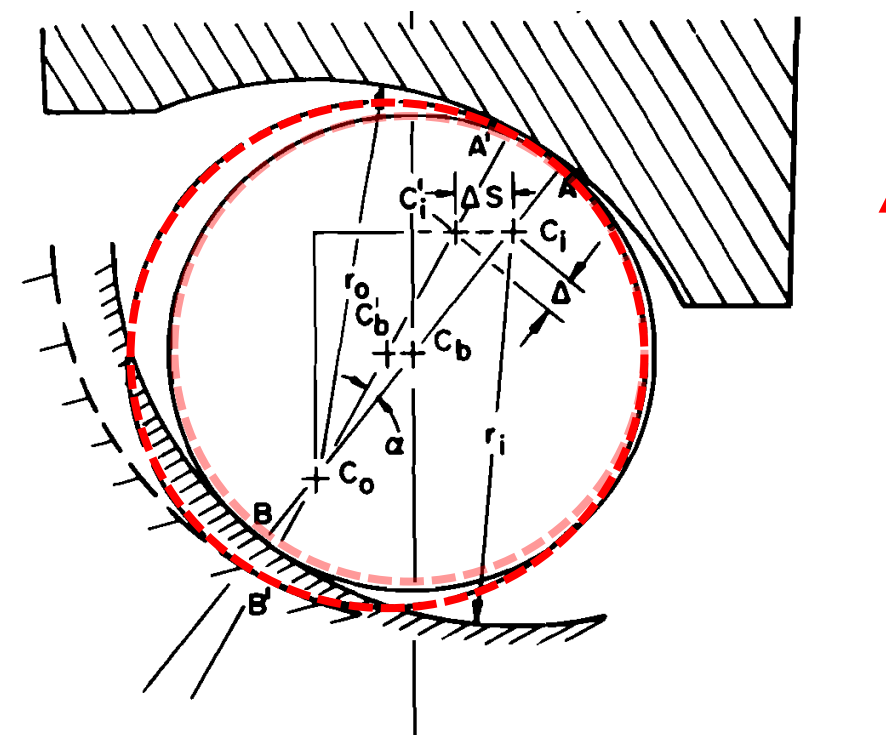
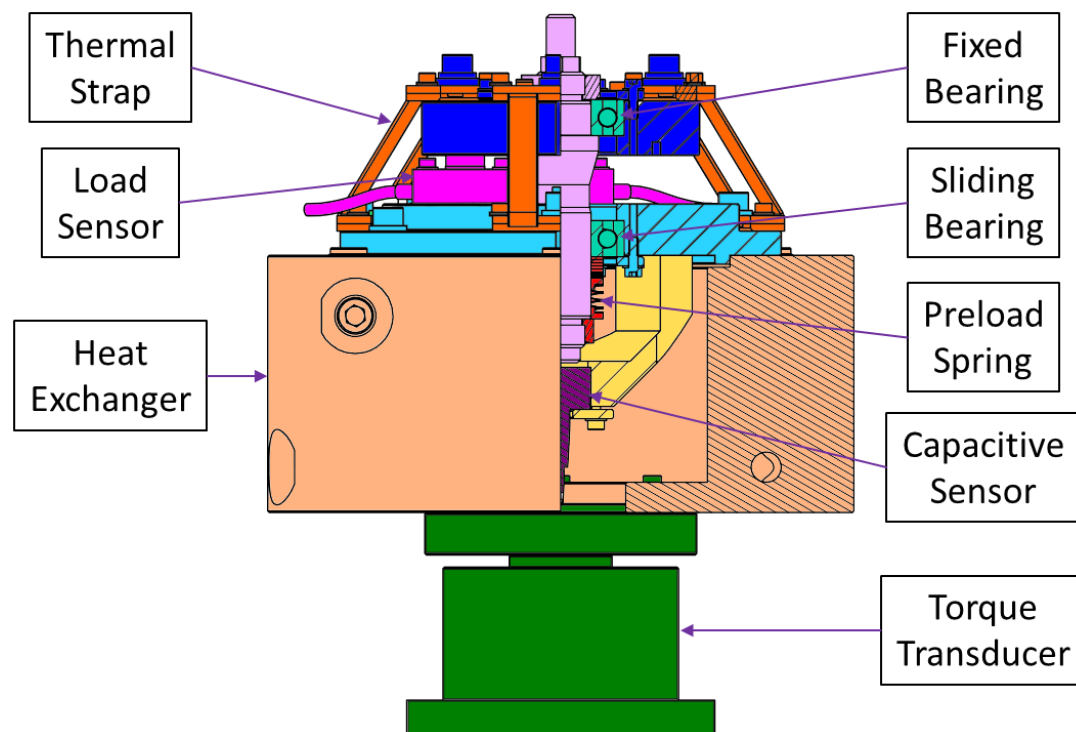
(Tyler et al, 1979, EHD Film Thickness Behaviour in DMA Bearings)

ABTR



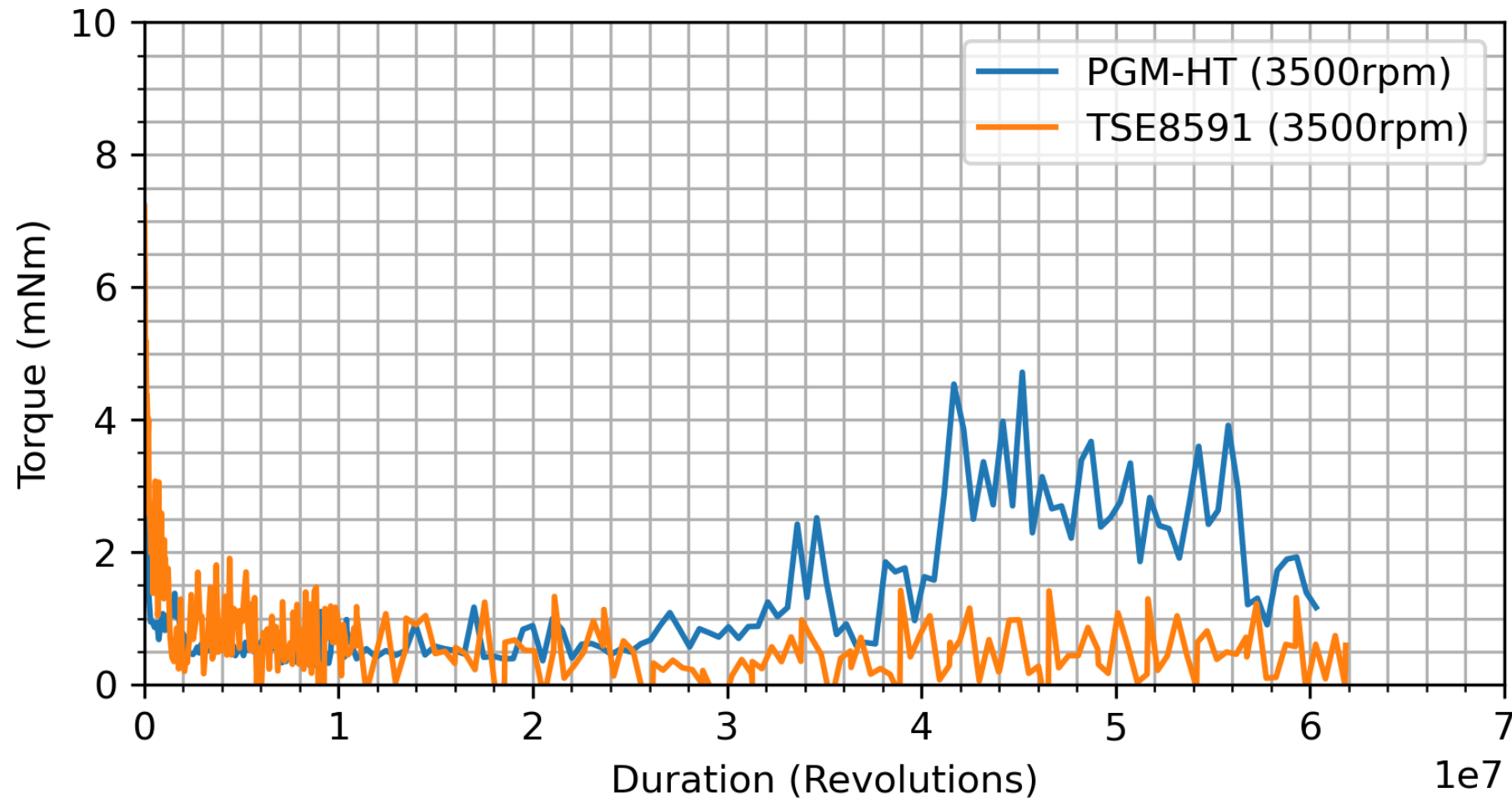
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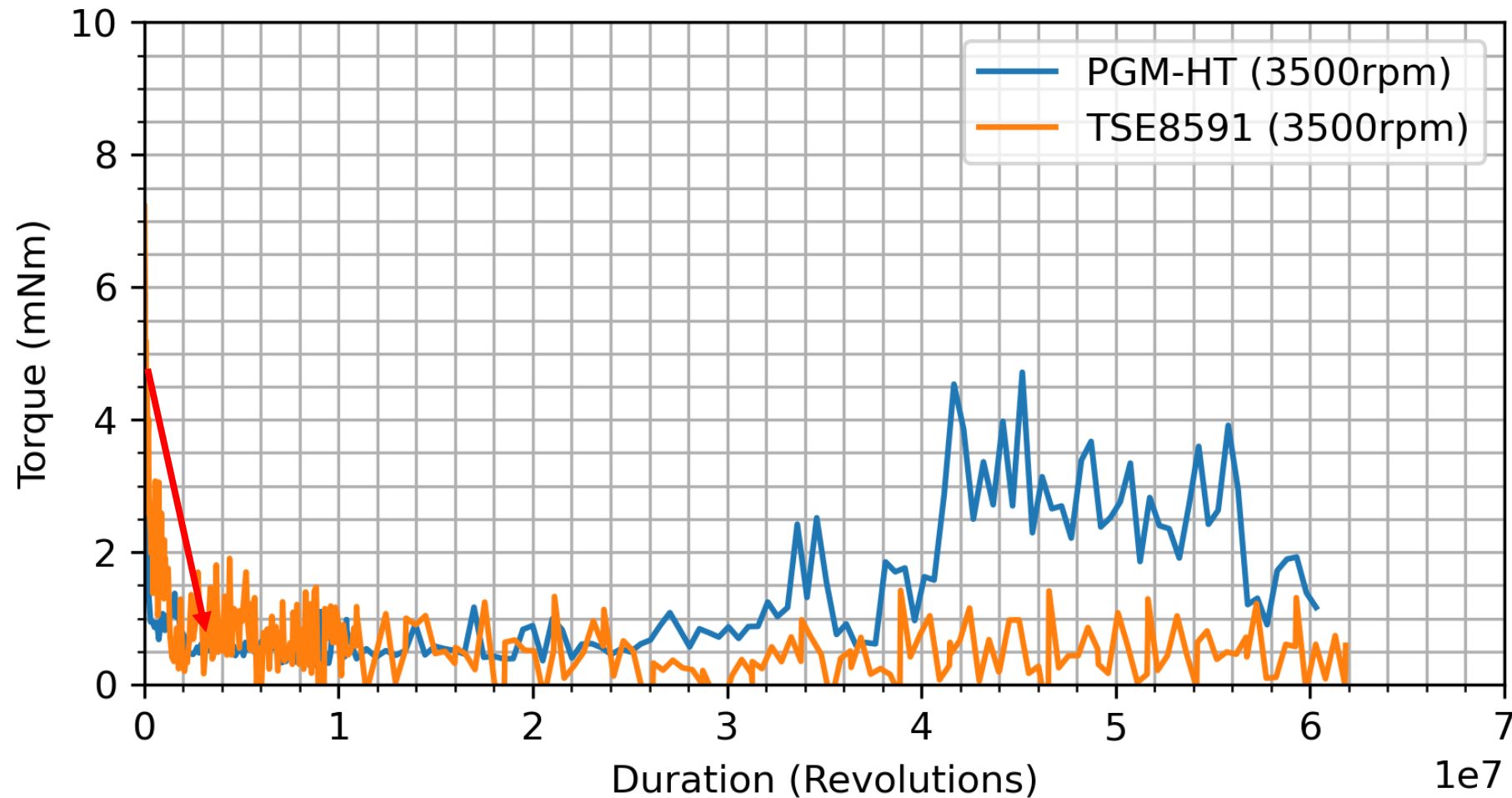


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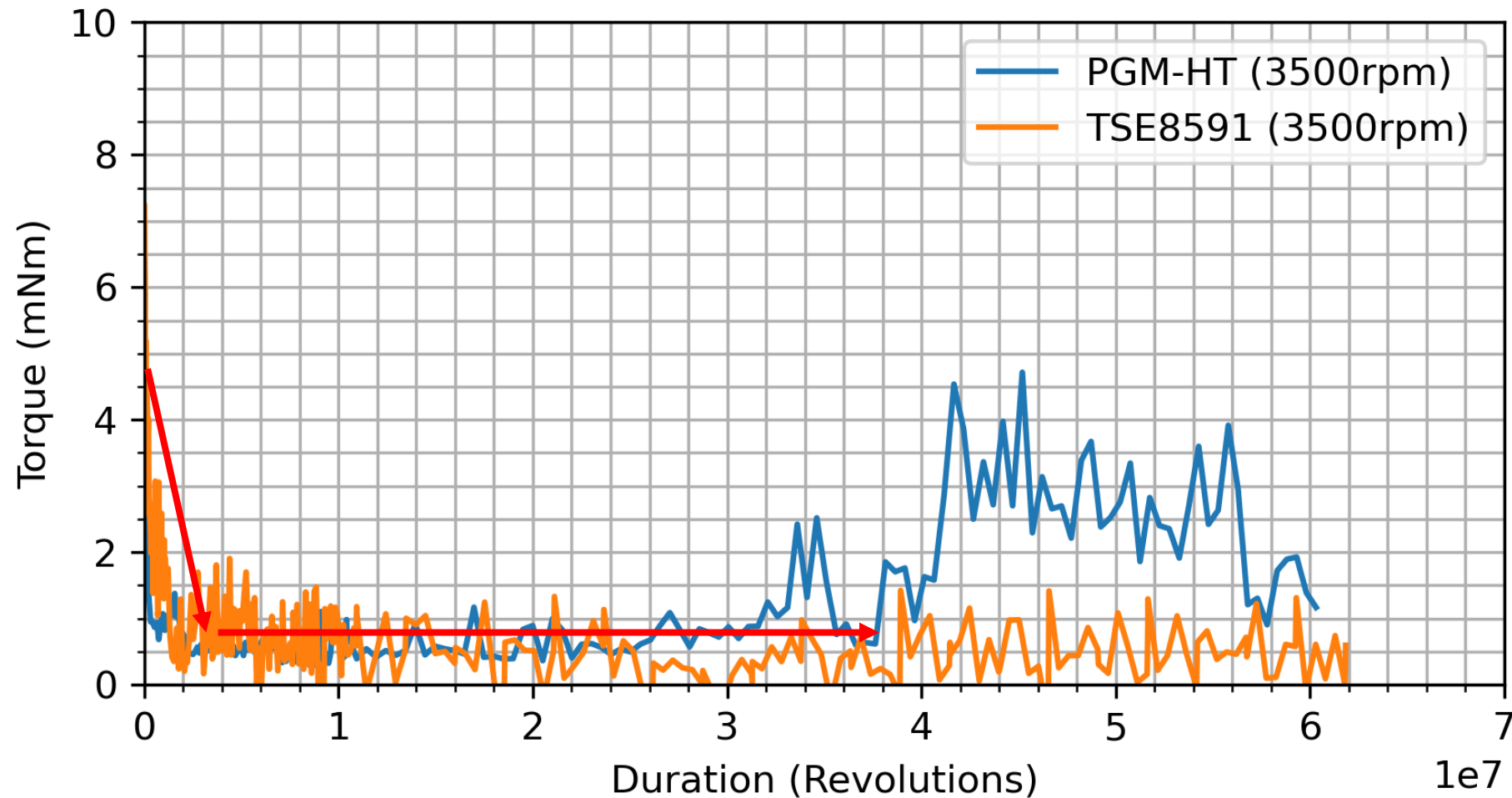
ABTR Test Results



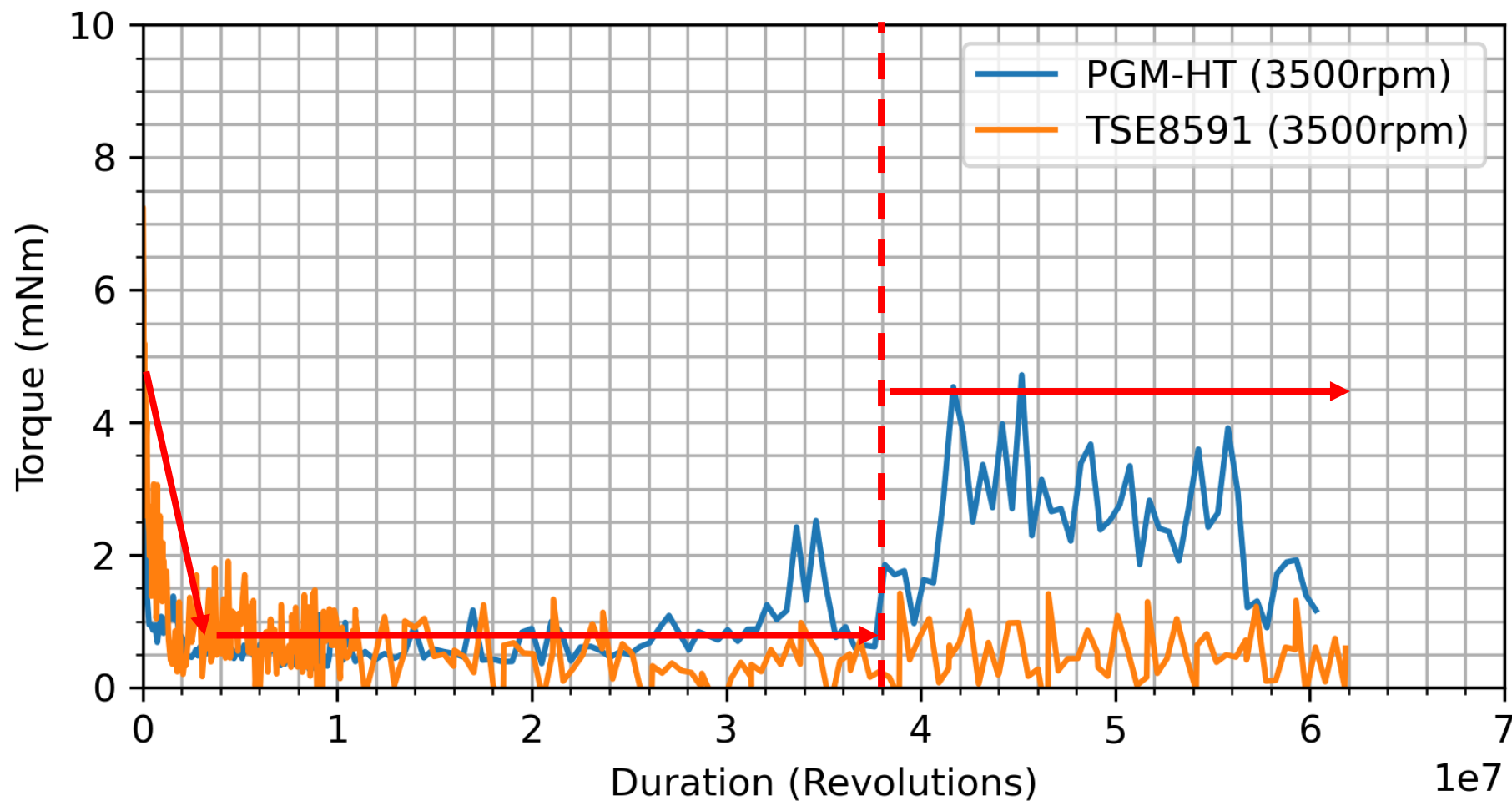
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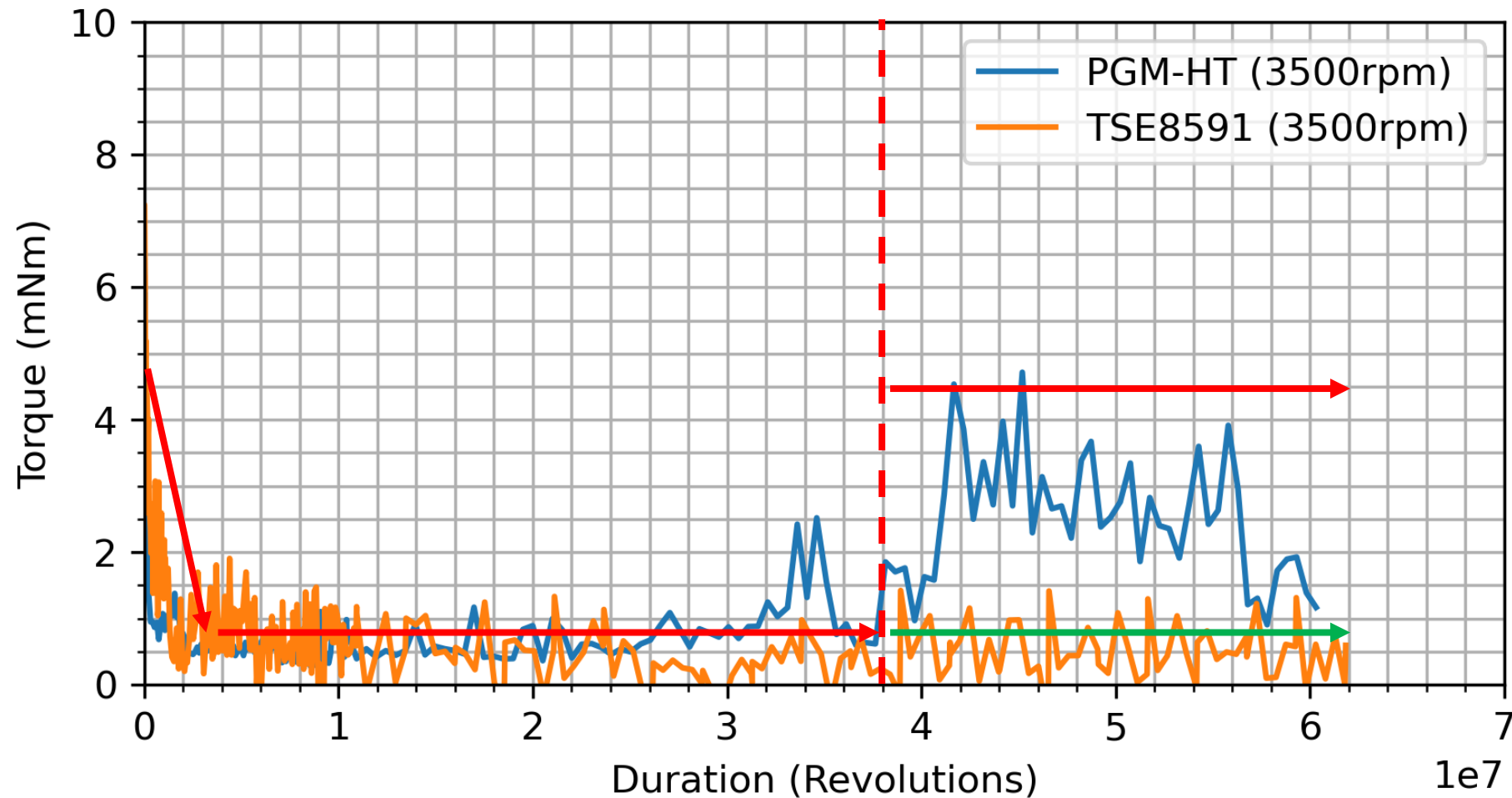
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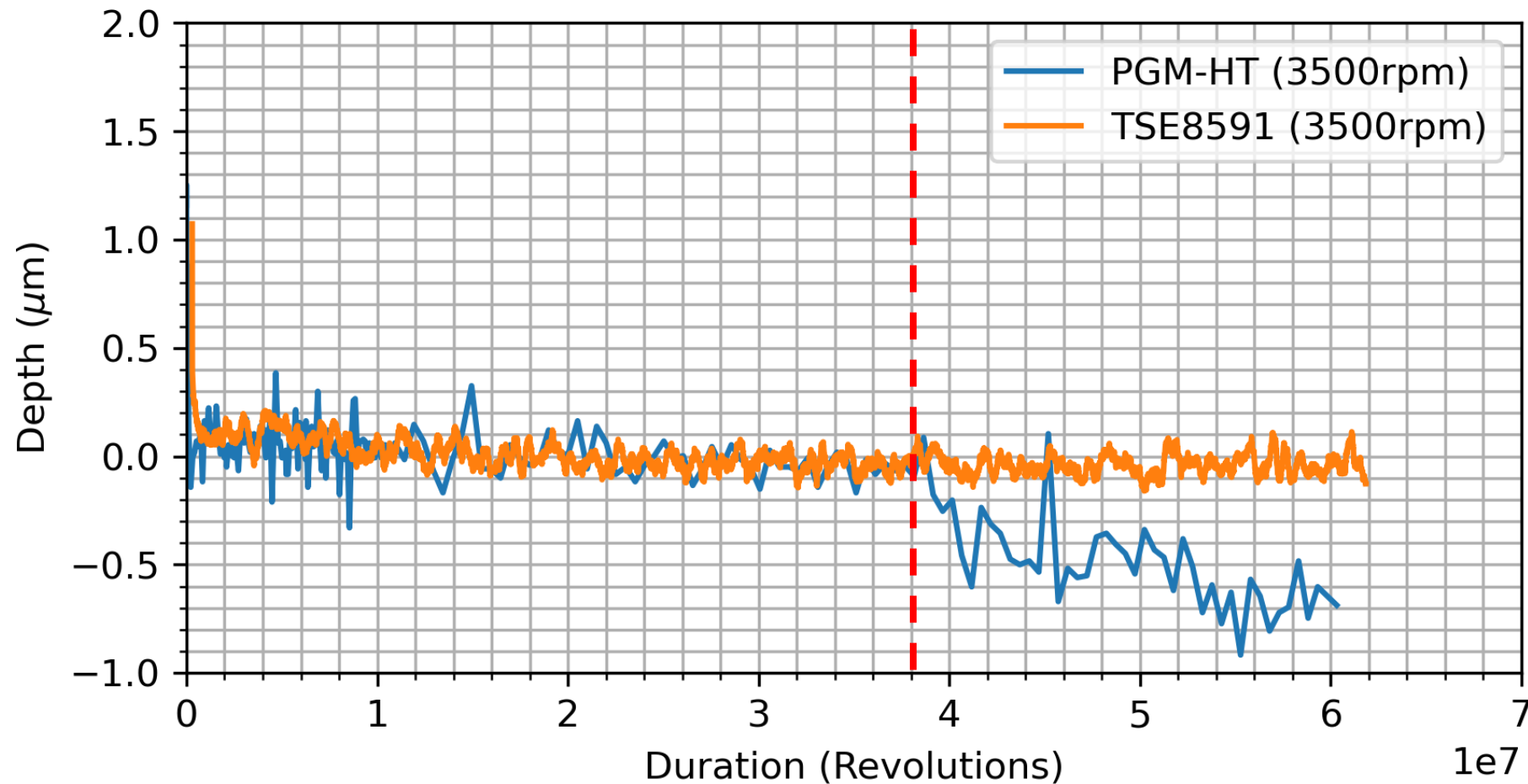
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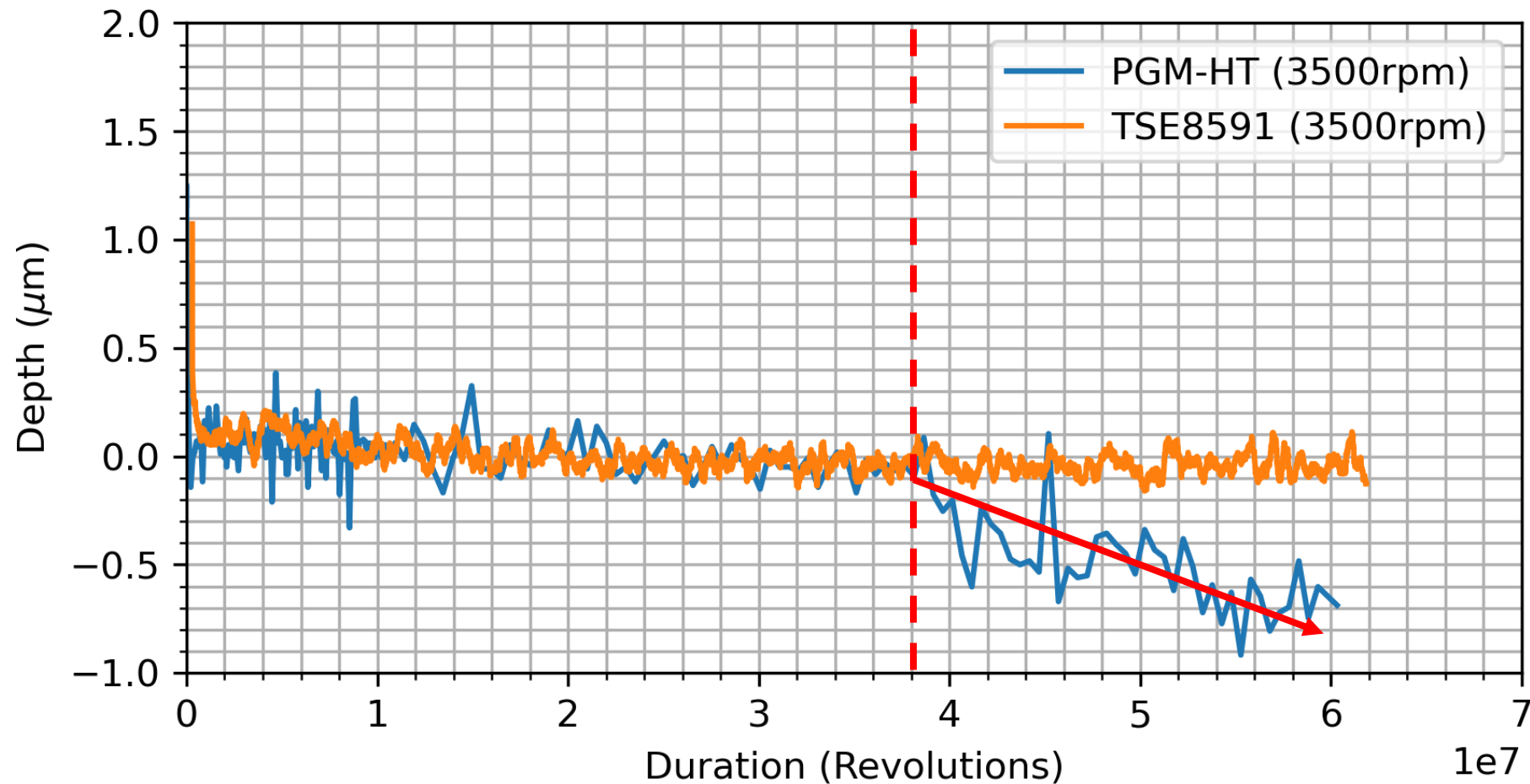
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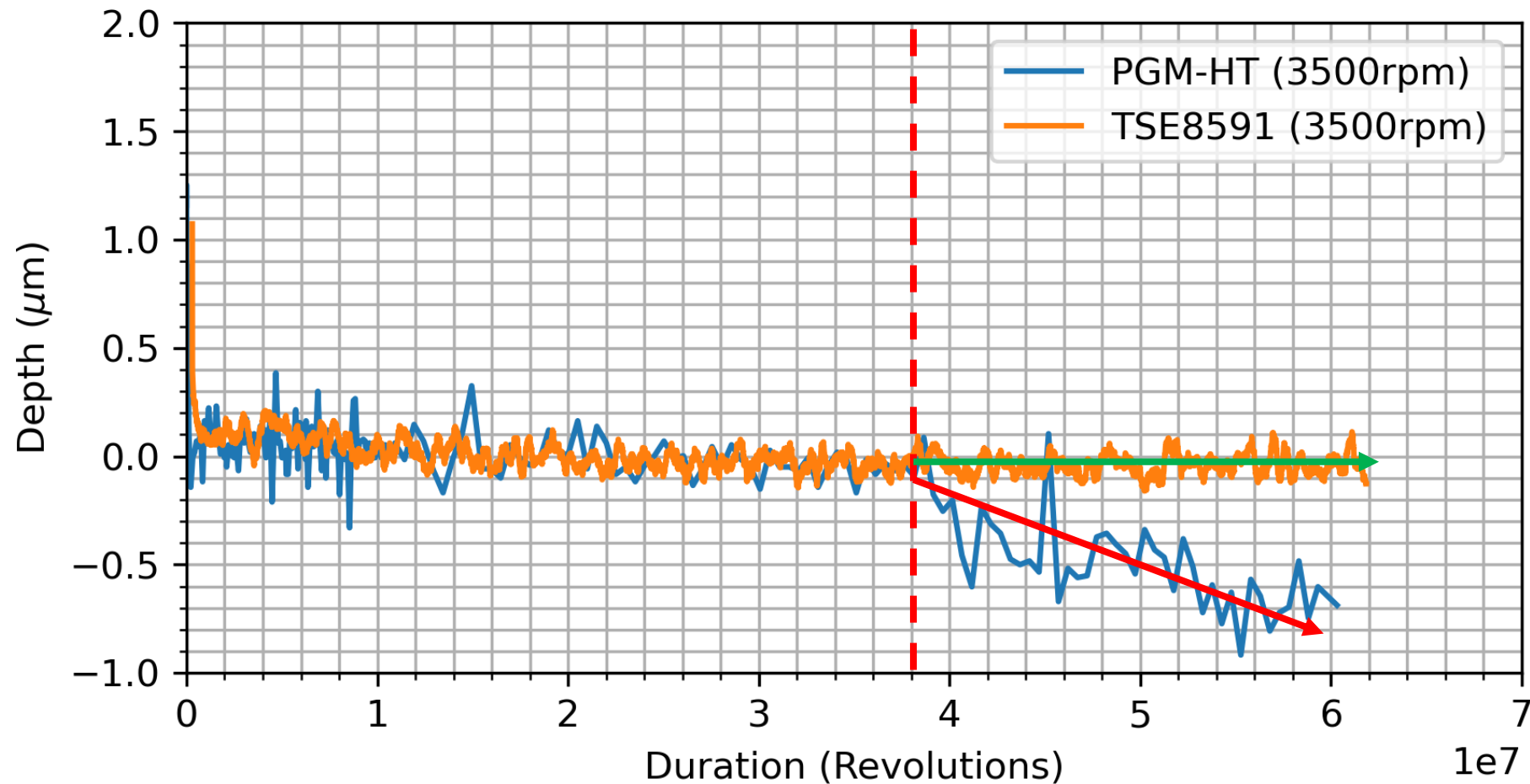
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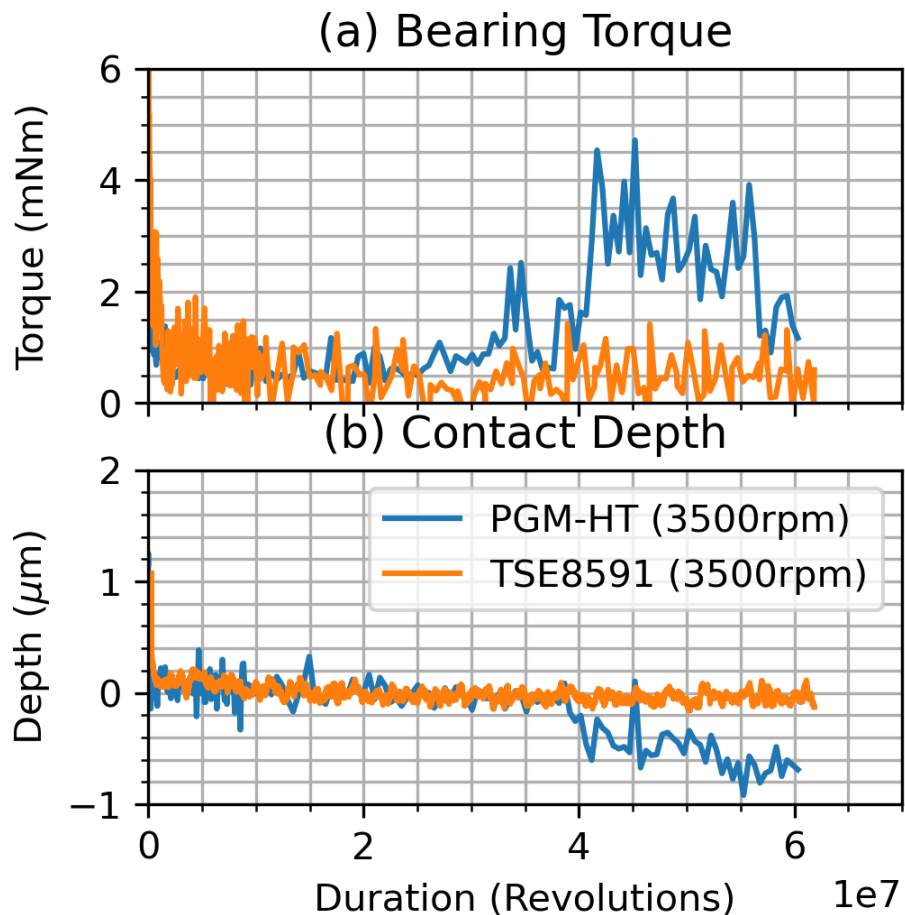
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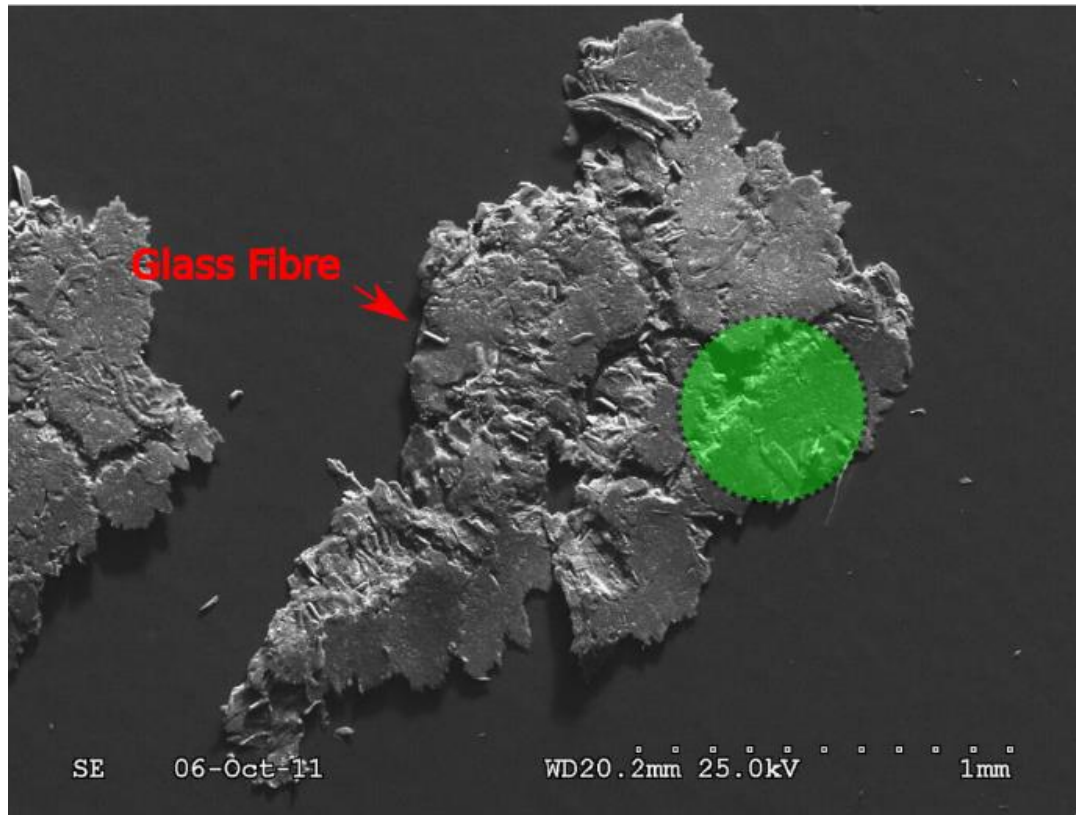


ABTR Test Results



- Clear difference in friction behaviour
- Change in friction behaviour accompanied by change in film thickness
- TSE8591 remains stable until the end of the test

Material Comparison



Parameter	Unit	PGM-HT	TSE8591
CoF	-	0.187	0.211
CTE (HT)	$10^{-6} / \text{K}$	63	65
Yield (HT)	MPa	5.10	5.60
Fibre Diameter	μm	~20	~3

(High Temperature (HT) data from AAC SLMC2 presentation from FPD 2020)

SLM Validation

Activity	PoD	SOT	Bearing
Assessment of new SLM sliding friction/wear properties			

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Conclusions

- SOT/ABTR are useful tools in the evaluation of SLMCs candidates.
- Facilities can be used to characterise transfer films in both a qualitative and quantitative manner.
- Testing shows that TSE8591 is a very encouraging candidate for replacing PGM-HT.

Acknowledgements

- ESTL acknowledge the following:
 - ESA TEC/MSM for project management and guidance
 - AAC/Ensinger for providing materials from SLMC project

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